



**Project :** Solar Park Enel 5 MW

**Position :** Solar Park Enel 5 MW

**Company :** Hydroplan

**Responsible :** Stelios Kalathakis

**Phone :**

**Facsimile :**

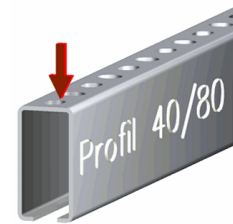
**E-Mail :**

**Profile type :** MPC Profile 40/80

**Profile length :** 3.304 [m] (Number of nodes : 71)

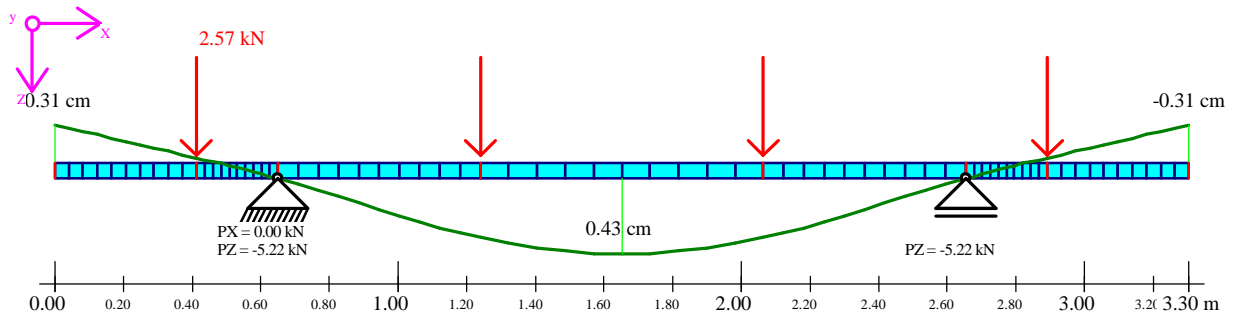
**Section values :**

Cross section :	5.820	[cm <sup>2</sup> ]
Weight :	4.680	[kg/m]
Youngs modulus :	210000.000	[N/mm <sup>2</sup> ]
Shear modulus :	81000.000	[N/mm <sup>2</sup> ]
Shear section :	Az = 4.620	[cm <sup>2</sup> ]
Resistance moment :	Wy = 10.182	[cm <sup>3</sup> ]
Inertia moments :	Iy = 40.727	[cm <sup>4</sup> ]



Ay =	1.110	[cm <sup>2</sup> ]
Wz =	9.092	[cm <sup>3</sup> ]
Iz =	18.184	[cm <sup>4</sup> ]

**System :** Vertical loads with own weight



**Input data :**

```

*****
*** Suspension conditions : 2 ***
*****
Position no.   PX PY PZ   MX MY MZ   MG   Marked
1             0.65000 21    1 1 1    0 0 0    0 1
2             2.65400 51    0 1 1    0 0 0    0 1

*****
*** Point loads      : 4 Max. value : 2.57380 [kN] ***
*****
Position no.   Px [kN]   Py [kN]   Pz [kN]   My [kNm]   Mz [kNm]
1             0.41300 11        2.57380
2             1.23900 31        2.57380
3             2.06500 41        2.57380
4             2.89100 61        2.57380

*****
*** Distributed loads : 0 Max. value : 0.00000 [kN/m] ***
*****
from position no. to position no.   Qz1 [kN/m]   Qzr [kN/m]   Qy1 [kN/m]   Qyr [kN/m]
0.00000 1 3.30400 71 0.04590 0.04590 (Own weight)
    
```

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```

*****
*** Element forces : Extreme values ***
*****
min. values :      N [kN]          Q [kN]          M [kNm]
max. values :      -0.00000 ( 1)   -2.61979 ( 51)  -0.61969 ( 21)
                  -0.00000 ( 1)    2.61979 ( 21)   0.91932 ( 36)

*****
*** Bearing loads : (*) Bearing force , (K) Point load ***
*****
Position no.      PX [kN]          PZ [kN]          MY [kNm]
0.65000  21      (*)          -5.22342 (*)          ( )
2.65400  51      ( )          -5.22342 (*)          ( )

*****
*** Anchor extraction forces : +F : Tension , -F : Stress ***
*****
Position no.      F1 [kN]          F2 [kN]          e [cm]

*****
*** Stress : extreme values ***
*****
min. values :      SigmaN [N/mm²]   TauQ [N/mm²]   SigmaM [N/mm²]
max. values :      -0.00000 ( 1)   -8.50580 ( 51)  -60.86093 ( 51)
                  -0.00000 ( 1)    8.50580 ( 21)   90.28891 ( 36)

Hint : TauQ=1.5*Q/A_bridge (shearing force take over only by bridge)

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*****
*** Structural analysis of stress in accordance with EC3 ***
*****

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```

Partial safety coefficient :      gamma-M = 1.100
Stretching limit :              fy,k = 235.000 [N/mm²]

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Load bearing combinations according to EC1

```

1.35 * Own weight + 1.35 * G
1.35 * Own weight + 1.50 * 0.90 * Q
- constant influences G
- changeable influences Q

```

Demands S,d

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SIGMA max = 1.35 * ( 90.289 + 0.000 ) = 121.890 [N/mm²] = Sigma_d
TAU max = 1.35 * ( 8.506 ) = 11.483 [N/mm²] = Tau_d

```

Demanding R,d

```

Limitation of direct stress= 235.000 / 1.10 = 213.636 [N/mm²] = Sigma_R,d
Limitation of shear stress= 213.636 / 1.732 = 123.343 [N/mm²] = Tau_R,d

```

Verification of bending and direct stress :

```

Sigma_d      121.890 [N/mm²]
----- = ----- = 0.571 <= 1.000
Sigma_R,d    213.636 [N/mm²]

```

Shear stress verification :

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Tau_d        11.483 [N/mm²]
----- = ----- = 0.093 <= 1.000
Tau_R,d     123.343 [N/mm²]

```

Comparable stresses do not need to be verified.

Hint :

If applicable, additional verifications of load bearing capacity and stability proofs need to be considered according to measures of corresponding literature or engineering standards !



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\*\*\*\*\*  
 \*\*\* Structural analysis in accordance with EC3 \*\*\*  
 \*\*\*\*\*

Partial safety coefficient :  $\gamma\text{-M} = 1.100$   
 Stretching limit :  $f_{y,k} = 235.000 \text{ [N/mm}^2\text{]}$

Load bearing combinations according to EC1  
 1.35 \* Own weight + 1.35 \* G  
 1.35 \* Own weight + 1.50 \* 0.90 \* Q  
 - constant influences G  
 - changeable influences Q

Demands E,d  
 $M_{E,d} = 1.35 * 0.919 = 1.241 \text{ [kNm]}$   
 $N_{E,d} = 1.35 * 0.000 = 0.000 \text{ [kN]}$   
 $Q_{E,d} = 1.35 * 3.930 = 5.305 \text{ [kN]}$

Demanding R,d  
 $M_{R,d} = 235.000 \text{ [N/mm}^2\text{]} * 10.182 \text{ [cm}^3\text{]} * 0.00100000 / 1.10 = 2.175 \text{ [kNm]}$   
 $N_{R,d} = 235.000 \text{ [N/mm}^2\text{]} * 5.820 \text{ [cm}^2\text{]} * 0.10000000 / 1.10 = 124.336 \text{ [kN]}$   
 $Q_{R,d} = 135.677 \text{ [N/mm}^2\text{]} * 4.620 \text{ [cm}^2\text{]} * 0.10000000 / 1.10 = 56.984 \text{ [kN]}$

Verification of strains of bending force and normal force :

$\frac{M_{E,d}}{M_{R,d}} + \frac{N_{E,d}}{N_{R,d}} = \frac{1.241 \text{ [kNm]}}{2.175 \text{ [kNm]}} + \frac{0.000 \text{ [kN]}}{124.336 \text{ [kN]}} = 0.571 \leq 1.000$

Verification of lateral forces

$\frac{Q_{E,d}}{Q_{R,d}} = \frac{5.305 \text{ [kN]}}{56.984 \text{ [kN]}} = 0.093 \leq 1.000$

Comparable stresses do not need to be verified.

Hint :

If applicable, additional verifications of load bearing capacity and stability proofs need to be considered according to measures of corresponding literature or engineering standards !

\*\*\*\*\*  
 \*\*\* Deflection : Extreme values \*\*\*  
 \*\*\*\*\*

max. values :  $UX \text{ [cm]} = -0.00000 \text{ ( } 0 \text{)}$   $UZ \text{ [cm]} = 0.43486 \text{ ( } 36 \text{)}$   $PhiY \text{ [rad]} = 0.00632 \text{ ( } 25 \text{)}$

\*\*\*\*\*  
 \*\*\* Check admissible deflection \*\*\*  
 \*\*\*\*\*

Standard field : 1  
 - Field length : 0.65000 [m]  
 - max. deflection : 0.30547 [cm]  
 - admissible deflection : 0.65000 [cm] (Cantilever L/100)

Verification of admissible deflection :

$\frac{f_{\text{available}}}{f_{\text{admissible}}} = \frac{0.305 \text{ [cm]}}{0.650 \text{ [cm]}} = 0.470 \leq 1.000$

Remark for adequacy verification:

Partial safety coefficient :  $\gamma\text{-F} = 1.000$   
 Partial safety coefficient :  $\gamma\text{-M} = 1.000$